

## Equation of State for Complex Liquid Mixtures

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The present work shows a successful extension of previous studies to molecular liquids for which the second virial coefficients are not known. Recent advances in statistical-mechanical theory of equilibrium fluids can be used to obtain an equation of state for compressed liquids. The average contact pair distribution function ( $G$ ), which is at the heart of the equation of state, has the very simple form of a single curve in  $\lambda b^* \rho^*$  (any substance). The effect of many-body forces may still be included in  $G$ . The temperature-dependent parameters in the equation can be calculated with reasonable accuracy for most practical purposes just from the experimental heat of vaporization and triple-point density. Thus, thermodynamic consistency is achieved by the use of two scaling parameters ( $\Delta H_v$ ,  $\rho_t$ ). In terms of these parameters, the reduced second virial coefficient ( $B_2^*(T)$ ) obeys a single law of corresponding states in which  $\alpha^*(T)$  and  $b^*(T)$  are only slightly modified. The correlations embrace the temperature range  $T_t \leq T < T_c$  and can be used in a predictive mode. The remaining constant parameters are best found empirically from  $\rho_t$  data for pure dense fluids. We tested the equation of state on several liquid mixtures. The results indicate that the density of liquid mixtures can be predicted within about 5% at any pressure and temperature.

Although reliable experimental data are always preferred over values obtained by estimation method, all too often reliable data are not available. The present result is remarkable because the only data used for estimating compressed liquid properties were the density and the heat of vaporization. The Clausius–Clapeyron equation provides a useful method for obtaining the enthalpies of vaporization from more easily measured vapor pressures. Liquid specific volumes are relatively easy to measure, and for most common organic liquids at least one experimental value is available. It should be noted that the accuracy is not necessarily enhanced by greater complexity.

An analytical equation of state, based on statistical-mechanical perturbation theory, has recently been proposed.<sup>1)</sup> This equation of state is quite accurate over the entire  $P$ – $\nu$ – $T$  ranges for all nonpolar or slightly polar fluids, including compressed liquids. Three temperature-dependent quantities are needed to use the strong principle: The second virial coefficient ( $B_2(T)$ ), an effective van der Waals covolume ( $b(T)$ ), and a scaling factor ( $\alpha(T)$ ), which is equivalent to the contribution to  $B_2(T)$  from just the repulsive branch of the intermolecular forces. The strong principle may also be characterized by three constants: the Boyle temperature ( $T_B$ ), the Boyle volume ( $\nu_B$ ), and an empirical constant reflecting the sphericity of the molecule. If the strong principle can be extensively used for molecular liquids, the practical question arises as to how to find the proper scale factors corresponding to  $T_B$ ,  $\nu_B$ , and  $\lambda$  in order that the strong principle can have real predictive power. The previous statistical-mechanical theory would take  $T_B$  and  $\nu_B$  from the experimental values of  $B_2(T)$ , the second virial coefficient of the vapor. However, the values of  $B_2(T)$  are hardly known experimentally for many compressed liquids of interest, the present method for finding a suitable scale factor, say, applying the cohe-

sive energy density, would be needed. The present study may be applied to real molecular liquids with no difficulties.

Agreement with measurements has been secured in that the material constants of the different systems and the adjustable constants in the expressions for the functionals have been made consistent with a vast number of experimental results. We recall that knowledge concerning the equation of state combined with that of the specific heat is equivalent to a fundamental equation from which all thermodynamic equilibrium properties can be calculated. An entire  $P$ – $\nu$ – $T$  surface is collapsed to a single curve; this result appears to hold with remarkable accuracy when tested with experimental data for any number of systems. We tested the equation of state of several liquid mixtures. The results show that the density of the liquid mixtures can be predicted within about 5% at any temperature and pressure.

In short, the purpose of this work was to correlate and to predict the behavior of complex liquid mixtures based on the latent heat of vaporization and the liquid density at the triple point, which are closely related to the cohesive energy density of regular solution theory. An empirical feature is incorporated in the corresponding-states principle, which enables it to describe the thermodynamic properties of mixtures at all liquid densities, temperatures, and compositions.

## Equation of State

We omit details concerning the statistical-mechanical perturbation theory derivation which have given elsewhere.<sup>2)</sup> The equation of state obtained by Ihm, Song, and Mason,<sup>1)</sup> including a small correction for attractive forces, has the following form:

$$\frac{P}{\rho K T} = 1 - \frac{(\alpha - B_2)}{1 + 0.22 \lambda b \rho} + \frac{\alpha \rho}{1 - \lambda b \rho}, \quad (1a)$$

where  $\rho$  is the number (molar) density,  $kT$  has its usual meaning, and  $\lambda$  is a constant. Three temperature-dependent quantities ( $\alpha(T)$ ,  $b(T)$ , and  $B_2(T)$ ) are needed to determine the equation of state for a real molecular liquid. The three parameters can be obtained from the internuclear potential ( $U(r)$ ) by integration:

$$B(T) = 2\pi \int_0^\infty \{1 - \exp[-U(r)/kT]\} r^2 dr, \quad (1b)$$

$$\alpha(T) = 2\pi \int_0^{r_m} \{1 - \exp[-U_0(r)/kT]\} r^2 dr, \quad (1c)$$

and

$$b(T) = \alpha + T \frac{d\alpha}{dT}. \quad (1d)$$

Here,  $U_0(r)$  is the repulsive part of  $U(r)$ ,

$$U_0(r) = \begin{cases} U(r) + \varepsilon, & r < r_m \\ 0, & r > r_m, \end{cases}$$

where  $\varepsilon$  is the depth of the potential well and  $r_m$  is the position of its minimum. If  $U(r)$  is known, it is straight-forward to calculate  $B_2(T)$ ,  $\alpha(T)$ , and  $b(T)$  from Eq. 1b—1d. Such calculations have been carried out by Song et al.<sup>3)</sup> for a Lennard-Jones (12,6) potential and for an accurate noble-gas potential. It fortunately turns out that  $\alpha(T)$  and  $b(T)$  are rather insensitive to the shape of the intermolecular potential, so that they appear nearly universal functions of temperature in terms of a suitable reducing unit, such as the heat of vaporization ( $\Delta H_v$ ) and the triple point density ( $\rho_t$ ). They are fitted as follows:

$$\alpha\rho_t = a_1 \exp[-C_1(RT/\Delta H_v)] + a_2 \{1 - \exp[-C_2/(RT/\Delta H_v)^{\frac{1}{4}}]\} \quad (2a)$$

and

$$b\rho_t = a_1 [1 - C_1(RT/\Delta H_v)] \exp[-C_1(RT/\Delta H_v)] + a_2 \{1 - [1 + \frac{1}{4}C_2(\Delta H_v/RT)^{\frac{1}{4}}] \exp[-C_2(\Delta H_v/RT)^{\frac{1}{4}}]\}, \quad (2b)$$

where the constants  $a_1$ ,  $a_2$ ,  $c_1$ , and  $c_2$  are  $-0.1053$ ,  $2.9359$ ,  $5.7862$ , and  $0.7966$ , respectively.

The central idea is to use second virial-coefficient data to determine the parameters for the corresponding states that are related to the scaling parameters,  $\Delta H_v$  and  $\rho_t$ . The resulting correlation can then be used to calculate  $B_2(T)$ , which is quite universal. The parameter  $\Delta H_v$  is determined from the experimental vapor pressure data using the Clausius-Clapeyron equation. It is remarkable that one functional ( $B_2^*$ ) does suffice for all nonpolar liquids, where,  $B_2^* = \rho_t B(T)$ . The values of  $B(T)$  are correlated as

$$B_2\rho_t = 0.4038908 - 0.076485 \left(\frac{RT}{\Delta H_v}\right)^{-2} - 0.0002504 \left(\frac{RT}{\Delta H_v}\right)^{-4}, \quad (2c)$$

where  $R$  is the gas constant. This correlation gives good second virial coefficients for different classes of substances up to the critical temperature ( $T_c$ ).<sup>4)</sup> The value

of  $\lambda$  can be obtained from Eq. 1a by fitting the  $\rho_t$  and  $\Delta H_v$  data. In summary, the correlation of the second virial coefficients ( $B_2$ ) requires only the scaling parameters  $\Delta H_v$  and  $\rho_t$ . The values of the parameter  $\Delta H_v$  were obtained indirectly by calculations based on the results of various vapor pressure measurements.<sup>5)</sup> It is important to stress that the present correlation operate in a predictive mode. The second virial coefficient is predicted over a much wider temperature range than that for which direct measurements exist.<sup>6)</sup> The  $\alpha^*(T)$  and  $b^*(T)$  are predicted over a similar wide temperature range, where  $\alpha^*(T) = \alpha(T)\rho_t$  and  $b^*(T) = b(T)\rho_t$ .

We can write the corresponding states result in the form

$$\frac{1}{G(b^*\rho^*)} \equiv \alpha^*\rho^* [Z - 1 + \frac{(\alpha^* - B_2^*)\rho^*}{1 + 0.22\lambda b^*\rho^*}]^{-1} = 1 - \lambda b^*\rho^*, \quad (3)$$

where  $Z = P/\rho kT$ ,  $\rho^* = \rho/\rho_t$ , and  $\lambda$  is the magnitude of the slope. The fact that  $\lambda$  also occurs on the left-hand side of this equation means that a successive-approximation procedure is needed to determine its value; usually, however, the triple-point density is sufficient because it is only in a correction term. We now wish to compare the theoretical result from Eq. 1a with the experimental data for molecular liquids. It is convenient to use the average contact pair distribution function ( $G$ ) defined in Eq. 3. The results for molecular liquids are given in Ref. 4, in terms of  $G$  and  $\lambda b^*\rho^*$  for any substance represented as a single curve. In other words in the corresponding-states treatment we solve. Eq. 3 for  $G(\lambda b^*\rho^*)$ , which is then treated as an unknown function to be determined from the experimental  $P$ - $\nu$ - $T$  data. The result turns out to be surprisingly simple,  $G(\lambda b^*\rho^*) \approx (1 - \lambda b^*\rho^*)^{-1}$ ; that is, a plot of  $G^{-1}$  against  $\lambda b^*\rho^*$  is very nearly a straight line whose slope is  $-1$ , the same for all values of  $P$  and  $T$ , so that the entire  $P$ - $\nu$ - $T$  surface of all nonpolar substances can be collapsed into single straight line by a suitable plot. In practice, only small deviations from accurate experimental results were found; a small adjustment was therefore applied to produce improved agreement.<sup>4)</sup>

The present correlation procedure can be generalized to mixtures of any number of components; a formal extension of Eq. 1a to mixtures can be written as<sup>7)</sup>

$$P/\rho RT = 1 + \rho \sum_{ij} x_i x_j (B_{ij} - \alpha_{ij}) F_{ij} + \rho \sum_{ij} x_i x_j \alpha_{ij} G_{ij}, \quad (4a)$$

where  $x_i$  and  $x_j$  are the mole fractions,  $F_{ii}^{-1} = 1 + 0.22\lambda b^*\rho^*$  and  $G_{ii}^{-1} = 1 - \lambda b^*\rho^*$ . The simplest combining rules for predicting unlike-molecule interactions from the like-molecule interactions are a geometric mean for  $\Delta H_v$  and an arithmetic mean for  $\rho_t$ . Thus, our combining rules would be

$$(\Delta H_v)_{ij} = [(\Delta H_v)_i (\Delta H_v)_j]^{\frac{1}{2}} \quad (4b)$$

and

$$(\rho_t)_{ij}^{-1/3} = 1/2[(\rho_i)^{-1/3} + (\rho_j)^{-1/3}]. \quad (4c)$$

Table 1. Volumetric Behavior of 0.5 Benzene +0.5 Hexane Liquid Mixtures

| T/K    | P/bar | Molar volume/cm <sup>3</sup> mol <sup>-1</sup> |        |       |
|--------|-------|--|--------|-------|
|        |       | COSTALD <sup>a)</sup>                          | Calcd  | Dev/% |
| 343.15 | 15.0  | 118.39   | 116.91 | 1.3   |
|        | 20.0  | 118.25   | 116.84 | 1.2   |
|        | 25.0  | 118.10   | 116.77 | 1.1   |
|        | 30.0  | 117.96   | 116.70 | 1.1   |
|        | 35.0  | 117.82   | 116.63 | 1.0   |
|        | 40.0  | 117.68   | 116.56 | 0.96  |
|        | 45.0  | 117.54   | 116.50 | 0.89  |
|        | 50.0  | 117.40   | 116.43 | 0.83  |
|        | 100.0 | 116.13   | 115.80 | 0.29  |
|        | 150.0 | 114.98   | 115.21 | -0.20 |
|        | 200.0 | 113.94   | 114.66 | -0.62 |
|        | 250.0 | 112.99   | 114.14 | -1.0  |
|        | 300.0 | 112.11   | 113.65 | -1.4  |
|        | 400.0 | 110.53   | 112.76 | -2.0  |
|        | 15.0  | 120.30   | 118.65 | 1.4   |
|        | 20.0  | 120.14   | 118.57 | 1.3   |
| 353.15 | 25.0  | 119.98   | 118.48 | 1.3   |
|        | 30.0  | 119.82   | 118.40 | 1.2   |
|        | 35.0  | 119.66   | 118.32 | 1.1   |
|        | 40.0  | 119.51   | 118.24 | 1.1   |
|        | 45.0  | 119.36   | 118.16 | 1.0   |
|        | 50.0  | 119.21   | 118.09 | 0.95  |
|        | 100.0 | 117.80   | 117.34 | 0.39  |
|        | 150.0 | 116.55   | 116.65 | -0.09 |
|        | 200.0 | 115.42   | 116.02 | -0.51 |
|        | 250.0 | 114.40   | 115.42 | -0.89 |
|        | 300.0 | 113.45   | 114.87 | -1.2  |
|        | 400.0 | 111.77   | 113.85 | -1.8  |
|        | 15.0  | 124.49   | 122.57 | 1.6   |
|        | 20.0  | 124.29   | 122.45 | 1.5   |
|        | 25.0  | 124.08   | 122.34 | 1.4   |
|        | 30.0  | 123.88   | 122.22 | 1.4   |
| 373.15 | 35.0  | 123.69   | 122.11 | 1.3   |
|        | 40.0  | 123.49   | 122.00 | 1.2   |
|        | 45.0  | 123.30   | 121.89 | 1.2   |
|        | 50.0  | 123.12   | 121.78 | 1.1   |
|        | 100.0 | 121.39   | 120.76 | 0.52  |
|        | 150.0 | 119.89   | 119.83 | 0.05  |
|        | 200.0 | 118.55   | 118.98 | -0.36 |
|        | 250.0 | 117.35   | 118.20 | -0.72 |
|        | 300.0 | 116.26   | 117.48 | -1.0  |
|        | 400.0 | 114.34   | 116.18 | -1.6  |
|        | 15.0  | 129.30   | 127.17 | 1.7   |
|        | 20.0  | 129.03   | 127.01 | 1.6   |
|        | 25.0  | 128.77   | 126.85 | 1.5   |
|        | 30.0  | 128.51   | 126.69 | 1.4   |
|        | 35.0  | 128.26   | 126.53 | 1.4   |
|        | 40.0  | 128.01   | 126.37 | 1.3   |
| 393.15 | 45.0  | 127.77   | 126.22 | 1.2   |
|        | 50.0  | 127.53   | 126.07 | 1.2   |
|        | 100.0 | 125.37   | 124.66 | 0.57  |
|        | 150.0 | 123.53   | 123.42 | 0.09  |
|        | 200.0 | 121.93   | 122.29 | -0.30 |
|        | 250.0 | 120.51   | 121.28 | -0.63 |
|        | 300.0 | 119.24   | 120.35 | -0.92 |
|        | 400.0 | 117.04   | 118.71 | -1.4  |

a) Corresponding States Liquid Density.<sup>8)</sup>

Table 2. Volumetric Behavior of Benzene+Octane Liquid Mixtures at 373.15 K and Six Compositions

| $x(\text{C}_6\text{H}_6)$ | P/bar | Molar volume/cm <sup>3</sup> mol <sup>-1</sup> |        |       |
|---------------------------|-------|--|--------|-------|
|                           |       | COSTALD <sup>a)</sup>                          | Calcd  | Dev/% |
| 0.0                       | 15.0  | 179.15   | 181.20 | -1.1  |
|                           | 20.0  | 178.93   | 181.10 | -1.2  |
|                           | 25.0  | 178.71   | 181.00 | -1.3  |
|                           | 30.0  | 178.50   | 180.91 | -1.3  |
|                           | 35.0  | 178.28   | 180.81 | -1.4  |
|                           | 40.0  | 178.07   | 180.72 | -1.5  |
|                           | 45.0  | 177.86   | 180.63 | -1.5  |
|                           | 50.0  | 177.66   | 180.53 | -1.6  |
|                           | 100.0 | 175.72   | 179.65 | -2.2  |
|                           | 15.0  | 162.57   | 164.45 | -1.1  |
| 0.20                      | 20.0  | 162.37   | 164.36 | -1.2  |
|                           | 25.0  | 162.17   | 164.27 | -1.3  |
|                           | 30.0  | 161.98   | 164.18 | -1.3  |
|                           | 35.0  | 161.78   | 164.09 | -1.4  |
|                           | 40.0  | 161.59   | 164.00 | -1.5  |
|                           | 45.0  | 161.40   | 163.91 | -1.5  |
|                           | 50.0  | 161.22   | 163.83 | -1.6  |
|                           | 100.0 | 159.46   | 163.00 | -2.2  |
|                           | 15.0  | 146.20   | 147.74 | -1.0  |
|                           | 20.0  | 146.03   | 147.66 | -1.1  |
| 0.40                      | 25.0  | 145.85   | 147.57 | -1.2  |
|                           | 30.0  | 145.68   | 147.49 | -1.2  |
|                           | 35.0  | 145.51   | 147.41 | -1.3  |
|                           | 40.0  | 145.34   | 147.32 | -1.4  |
|                           | 45.0  | 145.17   | 147.24 | -1.4  |
|                           | 50.0  | 145.01   | 147.16 | -1.5  |
|                           | 100.0 | 143.45   | 146.39 | -2.0  |
|                           | 15.0  | 130.06   | 131.10 | -0.79 |
|                           | 20.0  | 129.91   | 131.02 | -0.85 |
|                           | 25.0  | 129.76   | 130.94 | -0.90 |
| 0.60                      | 30.0  | 129.61   | 130.87 | -0.96 |
|                           | 35.0  | 129.46   | 130.79 | -1.0  |
|                           | 40.0  | 129.32   | 130.71 | -1.1  |
|                           | 45.0  | 129.17   | 130.64 | -1.1  |
|                           | 50.0  | 129.03   | 130.56 | -1.2  |
|                           | 100.0 | 127.69   | 129.85 | -1.7  |
|                           | 15.0  | 114.16   | 114.57 | -0.35 |
|                           | 20.0  | 114.03   | 114.49 | -0.41 |
|                           | 25.0  | 113.90   | 114.42 | -0.46 |
|                           | 30.0  | 113.78   | 114.35 | -0.50 |
| 0.80                      | 35.0  | 113.66   | 114.28 | -0.54 |
|                           | 40.0  | 113.54   | 114.21 | -0.59 |
|                           | 45.0  | 113.42   | 114.14 | -0.63 |
|                           | 50.0  | 113.30   | 114.07 | -0.67 |
|                           | 100.0 | 112.18   | 113.41 | -1.1  |
|                           | 15.0  | 98.49  | 98.22  | 0.27  |
|                           | 20.0  | 98.39  | 98.15  | 0.24  |
|                           | 25.0  | 98.29  | 98.09  | 0.21  |
|                           | 30.0  | 98.19  | 98.02  | 0.17  |
|                           | 35.0  | 98.10  | 97.96  | 0.15  |
| 1.0                       | 40.0  | 98.00  | 97.89  | 0.11  |
|                           | 45.0  | 97.90  | 97.83  | 0.08  |
|                           | 50.0  | 97.81  | 97.76  | 0.05  |
|                           | 100.0 | 96.91  | 97.15  | -0.24 |

a) Corresponding States Liquid Density.<sup>8)</sup>

Once  $(\Delta H_v)_{ij}$  and  $(\rho_t)_{ij}$  are known, the values of  $\alpha_{ij}$ ,  $b_{ij}$ , and  $B_{ij}$  follow from Eqs. 2a, 2b, and 2c as for pure substances. The quantities  $G_{ij}$  and  $F_{ij}$  for mixtures are given elsewhere.<sup>7)</sup> We had to test the combining rules given by Eqs. 4b and 4c, on compressed liquid mixtures. The results show that the density of liquid mixtures can be predicted within 5%. These are shown in Tables 1 and 2.

### Results and Discussion

The previous statistical-mechanical theory would take  $\varepsilon$  and  $r_m$  based on the experimental values of  $B_2(T)$ , the second virial coefficient of the vapor.<sup>2)</sup> However, since  $B_2(T)$ , would not be known experimentally for many compressed liquids of interest, this method for finding suitable scale factor would be needed. The present work shows how the equation of state of a compressed liquid can be given a statistical-mechanical basis; this method is needed for applications to real molecular liquid mixtures. The  $P$ - $\nu$  from our two-parameter equation of state are given in Tables 1 and 2. The values were calculated from Eq. 4a using Eqs. 2a, 2b, and 2c in conjunctions with Eqs. 4b and 4c. The agreement is fairly good. We repeat that Eq. 2 would be needed when the values of  $B_2(T)$  are not experimentally known for most of the compressed liquids of interest.

The most important aspect of the present work is that the linear  $\lambda b^* \rho^*$  dependence of the  $G^{-1}$  of any liquid can be given a strong basis in statistical mechanics. Moreover, the  $G$  can be calculated if  $\Delta H_v$  and  $\rho_t$  are known. The present work also shows to what extent the results for compressed liquids can be extended, namely from critical up to the freezing density. This work shows useful (predictive) applications to real molecular liquid

mixtures. The procedure has been tested on liquid mixtures ranging in complexity from benzene+*n*-hexane to benzene + *n*-octane.

In summary, although theory indicates that  $G$  is a function of a single variable ( $b^* \rho^*$ ) for pure substance, the fact that  $G^{-1}$  is nearly linear in  $b^* \rho^*$  is empirical, and the numerical value of  $\lambda$  must be found from  $\rho_t$ . Furthermore, our equation of state appears to give accurate  $P$ - $\nu$ - $T$  results at all liquid densities and temperatures. It is also simple in form and easy to use in a practical sense.

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